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# (54) WASHING METHOD FOR SILICON WAFER

(57) Abstract:

PURPOSE: To obtain a silicon wafer having high cleanliness by washing this silicon wafer by using an aq. soln. contg. hydrogen fluoride and contg. a specific oxidizing agent as a detergent.

CONSTITUTION: The aq. soln. contg. 0.1 to 20wt.% hydrogen fluoride and contg. the oxidizing agent described below as the detergent is used at the time of washing the silicon wafer. (i) 0.5 to 25wt.% sulfuric acid or (ii) 0.05 to 10wt.% hydrogen peroxide or (iii) bubbles of an oxidative gas are used as the above mentioned oxidizing agent. Gases contg. oxygen and nitrogen suboxide are usable as the oxidizing gas. Ultrapure water is used as the solvent. The evaporation of the hydrogen fluoride and the water and the evaporation decomposition of nitric acid are accelerated and the compsn. of the washing liquid may deviate from the range of this method if the washing temp. is increased to more than a necessary high temp. Further, the heating up takes time and such may drastically impair workability and, therefore, the heating up to 80°C is more preferable.

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◎発明の名称

シリコンクエハの洗浄方法

**倒特 顕 平2-3386** 

**愛出 願 平2(1990)1月12日** 

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し、英男の名称

シリコンウェハの教修方法

- 2.特許請求の範囲
- (1) クリコンウェハを放停するに関し、0.1 ~20 度量%の分化水器を含有し、かつ酸化剤として、0.5~25 医菌光の硝酸を含有する水溶液を洗浄療 とすることを特殊とするシリコンウェハの作停方 法。
- (2) シリコンウェハを秩序するに際し、9.05~10 重量%の亦化水果を合みし、かつ酸化剤として 9.05~10重量%の過酸化水果を合有する水解液を 洗棒球とすることを斡旋とするシリコンウェハの 発序方法。
- (3)、シリコンウェハを兼称するに関し、6.05~10 重量%の形化水素を含有し、かつ酸化剤として酸 化性ガスの気速を提入せしめた水溶液を表体設と することを特徴とするシリコンウェハの洗井方 法。
- 3.免明の詳細な説明

産業上の利用分野

本発明は、シリコンウェハの表面を高角声な状態にするための式声方法に関するものである。 従来の改得

近年、デバイスの高泉積化に停って、その基影となるシリコンウェハの表面をより一般破跡化することが強く望まれている。

シリコンクェへの表面に、シリコン粒子や腐瘍の世枝千行染物質(パーティクルとも言われる)が存在すると、デバイス程線の筋線やシェートの類固となり、温琴金属等の金属系汚染物類があると、酸化諸超級婦女筋の発生やライフタイムの低下といった問題が生じる。このため、これら汚染物質を独立するための抗疫が行われるが、発酵の際に形象されることも避けなければならない。

要款のシリコンウェハの税債方法としては、 ① 希邦時水溶液で洗浄する方法、②塩酸または硫 能と適能化水面との混合水溶液で洗浄する方法、 および③アンモニアと適時化水流の混合水溶液で 洗浄する方法が行われている。これら名洗浄法で

#### **销册平3-208900 (2)**

使用される独身級には、数数子均失物数や分属基 存業能質を極力過減した認施度の変品額や水が使 用されている。

従来の税券方法のうち、①はシリコンウェハ表 頭に造場10人程度の厚さで存在する自然酸化緩を 紹用する能力を有し、磁化膜中の金属系円染物質 の除去効果は高いが、単粒子汚染物質の低級は難 しいという簡数がある。

少は塩酸または塩酸が持つ全国系汚染物質に対 する高度解能力を利用したものであるが、酸化酸 を溶解する能力がない。このため、酸化酸上の全 風光丹気物質を飲出する効果は高いが、酸化酸中 少酸化鞣とシジョンの界面に存在する金属系汚染 物質を除去する効果は低い。

毎はシリコン目身を潜解する働きがあるため、 その上に存在する金属系形突物質を除去する効果 は高いが、 塩基性の洗浄液中で生成する静化膜は 洗浄液中の金属系形突物質等を取り込み高いとい う性質があり、シリコンウェバが河行味される可 能性が高い。しかし、この方法は微粒子の給去効

したがって、スタイトニッチ生でもシリコンウェ ハの高資体化には世界があると言わざるを元ない。

#### 恐頭が解決しようとする設調

太陽明は、シリコンウェバを抜掛するに駆して、Pe等の金属市所染物質的表がよび低粒子消染物質を振りて低減し、健化液経域層欠難の発生やライ

張が高いため、ウェバメーカーやデバイステーカーで広く利用されている。

また、上部従来法の問題点を解消する方法として、60重要%の組織と 6.1型更%以下の赤化水支の混合水溶液中にシリコンケェハを製造して復みするステイトエッチ法と呼ばれる万法が提案されている。(Ritus Takizova 5. "Estended Abstracts of Solid State Barises and Materials"、1988年、P.475)。

しかし、本海体用グレードと呼ばれる最高純度の消散でも、ppb オーダーまたはサブppb オーダーの会議系持知物質にとえば起、Ca、Fe、K、Pa、24年が含まれているので、60金量がもの路震度の消散を含む炎が近中の会議系得集物質の速度は高く、また石英ガラス製の炎浄性を使用すると石英ガラス中の金属不純物が部出して、その存成はますます時まる。

をして、高波波角酸の強い酸化力でシリコン ウェハの妄屈に酸化酸が形成され、洗移療中の金 競系形染物質が酸化膜やに取り込まれ易くなる。

フタイムの低下といった品質問題がなく、かつデ パイスにした場合の電気特性の労免もない高額枠 匿のシリコンウェハを得ることを目的とする。 課題を解決するための手段および作用

水苑明の質旨はつぎのとおりである。

- (1) シリコンウェハを沈持するに数し、 6.1~20 重量%の売化水県全合村し、かつ酸化剤として 8.5~25度量%の明酸を含有する水溶線を洗浄値 とすることを特徴とするシリコンウェへの洗浄力 注。
- (2) シリコンウェハを沈わするに関し、6.65~16 重量%の亦化水実を含むし、かつ酸化剤として 6.65~10度量%の過酸化水滑を含むする水容温を 沈神波とすることを特別とするシリコンウェバの 沈神方法。
- (3) シリコンウェハを洗浄するに関し、0.05~80 重量%の角化な異を合称し、かつ酸化物として酸 化性ガスの気部を退入せしめた水溶液を洗浄液と することを特徴とするシリコンウェハの抗浄方

#### **转扇平3-208900 (2)**

本登明法は、シリコンウェハを依存するに際期し、抗存被すの不納物を優力気減するために選問の最終を使用する。すなわち、太急男法は、必要を使用する。すなわち、太急男法は、必要を使用する。すなわち、太急男法は、必要を使用する。すなもの、大きのののが免疫を受けません。シリコンに対するニッチング能を対し、対し、おいては必要を小限の過度を使用し、決定のの過度を使用し、決定のでは必要を小限の過度を使用し、決定のでは必要を小限の過度を必要を開けます。

本角明技において、税券破中の事化水素、硝酸 および過酸化水素の強度は、それぞれ RP、 B B O , 、 および B O , としての重要 20 である。 請求項(2) に おいては、酸化性ガスとして酸素および亜酸化 会業 (一件化二室実) 等を含むガスを使用することができる。 また、 溶媒としては熔純水を使用する。

調でかつ過酸化水素が6.05分型%火燥だと、金属系汚染物質の除去物果が不充分である。 お化水 类の 遺居 を増して10距 最初を越えると、シリコンウェハの変面に散 粒子形染物質が増加する傾向が おめられる。また過酸化水素の濃度を増して10重 最初を結えると、シリコン実面のエッチング最が 過大になってウェハ表剤が貫化で参った状態になる。 そして、非化水素が10重量%以下では、薬剤から殺入する不能物の過度は実質上周期ない。

したがって、現化水素の高度を0.05~10重量が、 過酸化水果の高度を0.05~10重量がとした。 な お、洗浄温度については、80℃を終えると洗浄む らが生じて熱処理後のシリコンウェハ表面にピッ ト状ケ路を対起するおそれがあるので、80℃以下 とするのが望ましい。

語求項(3) において、患化水突が6.05愈量%会 調でかつ酸化性ガスの気能を収入させない場合は 企屋不巧笑物質の鉄土効果が不免分である。 非化 水海の濃度を増して10番量%を越えると、シリコ 請求快(1) において、発化水変が 6.3 重異名 未 請でかつ前限が 6.5 重量分末繋だと、金属系符染 物質の快去効果が不充分である。非化永素の複複 を増して20重量分を越えると、シリコンクェハの 表面に数粒子行染物質が増加する傾向が認められる。また前離の環境を増して25重量分を越える と、シリコン表面のエッチング最が過大になって ウェハ表面のエッチング最が過大になって ウェハ表面のエッチング最が過大になって では、素別から認入する不動物の環境は変質上 問題ない。

したがって、赤化水黄の譲渡を 6.1~26頭最外、 研飲の譲渡を 0.5~25頭最分とした。なお、枕珠 程度については、必要以上に高温にすると赤化水 素および水の蒸気や消費の高見分解が促進されて 次体液の組成が水発明の範囲から外れるおそれが あり、さらに早間に時間がかかり作業性を楽しく 治なうようになるので、80℃以下とするのが迸ま しい。

請京項(2) において、弗化水器が8,05重量%来

ンウェハの製画に放柱子行業物質が増加するとともにエッチング量が過去になってウェハ表面が荒れる。そして、魚化水業が10番量が以下では遅期から脳入する不純物の譲渡は実費上問題なく、また雌化性ガスは不純物譲渡の海めて低い高齢度のものが比較的容易に得られるので問題ない。

したがって、売化水宝の設度を9.05~20重量が とし、酸化剤として飲化性ガスの気流を調入せし のることとした。なお、技術温度については、 88でを越えると洗浄むらが生じて熱処理後のシリ コンウェハ表面にピット次欠物を誘起するおそれ があるので、88で以下とするのが望ましい。

美物館に酸化性ガスの気想を選入せらめるには、 洗浄油内にガス導入管を入れてパブリングさせるか、 めるいは発浄地の底部にガス吸出孔を設けてパブリングさせる等の公知の手段を採用することができる。

本是明語によれば、シリコンと矛葉イオンとの 間に生じるシリコンのアノード溶解反応と、酸化 剤の起こすカソード反応とが電気化学的にカップ

#### **销期平3-208900 (4)**

ルして決められる異女鬼位がアノード部になるので、シリコンウェハ表因の金異系乃染物質が除去 されやすい。

本発明社の範囲の参案イオンを含む強微性の本格 減中ではシリコン酸化物からなる不懈整度膜が 化学的または電気化学的に溶解し、シリコンウェ へ表面が初の状態になるため、酸化剤が必要量型 加されて実食電位がアノード側になるとウェへ表面の金属系行染物質が容易に原虫される。

なお、水英明法において、挽物液の成分として 上記以外のもの何えば多化アンモニウム等の場像 を洗剤症に採加したとしても洗剤能力が損なわれ ることがない。

さらに、本発明法において、使来公知の残事法 と組み合わせて行ってもよい。例えばアンモニア と過齢元太美の退合太弱娘で乾浄し、さらに効果 酸水部頭で残浄した後、本発明法により乾季する とより効果的である。

#### 突热例

(1) 結束項(1) の災処例

水性であるかも巨視により利足し、耐水性であるものも〇日、やや成水性であるものを今日、根本性であるものを×日で表示した。破水性であればシリコンウェへの表面にはシリコンの酸化物すなわら酸化製が存在しないことを示す。

さらに、光学類放棄によりウェハ表面のビット 状欠略のお気を観覧して表示した。ピット状欠略 なしは、エッテング量が過正で緩めて平荷な練頭 状態の表面をおしていることを示している。

第1 表において、比較例の相の.18まびNo.15 は 先化水素が少ないため毎にFeおよびCaの液存量が 多く、四 じくNo.8およびNo.14 はあ化水度が多す ざるためピット状欠陥が生じるとともに観粒子符 染物質が成存した。また、比較例のNo.19 および No.26 は発酸が多すざるためピット状欠陥が生じ た。

使来例のBa.21 ステイトエッテ族はBBO: 89重 量料、HF:0.1重量%の水溶液で改体したものであ るがFaの除去効果が低い。8a.22 アンモニア過酸 化水果法は 8b.14.1重量%、BO:4.4能量%の水 的 270×10% atoms/cm² のCr. 約 240×10<sup>10</sup> atoms/cm² のCr. 約 240×10<sup>10</sup> atoms/cm² のPsおよび約 312×10<sup>10</sup> atoms/cm² のPiにより表面が特別されたシリコンウェハを、第 1 表に示する機能 建設に被援して洗浄した結果を同談に示す。洗浄 後のシリコンウェハは、直ちに危険水中で5分間以上の液水水気を2回行が、スピンドライヤーにより能減した後、表面の形染金属の分析に共した。

分析は、視別的政府戦によりシリコンフェへの 安婦 1 A mを化学エッチングして溶解し、放業無 級中の会歴元素戦度をフレーAレス原子吸光光度 分析法により足量した。なお、版中のNDは分析定 是下限以下であることを示し、Crix 9.1×10<sup>80</sup> atoms/cm<sup>2</sup> 未満、CoのよびFeは 9.2×10<sup>84</sup> atoms/cm<sup>2</sup> 未満、Niな 2.8×10<sup>80</sup> atoms/cm<sup>2</sup> 未摘である。

ウェハ表面の数粒子は、ウェハ表面微粒子計類 製量により御定し、10個/ウェハ以下をOB、 10個/ウェハ磁を×印で表示した。

また、花巻後のウェハ表面が疎水池であるが観

太是明朝(1) は、何れもシリコンウェハ変菌の 最近千乃染物質がよび全属系行染物質が描めて感 減され、乳炸染の表面にピット状欠階をない。ま た染作後の裏面に比較化態が存在せず、資水性の 表面状態になっている。これは、乳炒中に酸化果 が形成されてその中に栽渉策中の金属系行染物質 が取り込まれるという洗炒による再乃飲が、本発 明例(1) では生じていないことを意味する。

[2] 請求項(2) および請求項(3) の実施例

約18×10<sup>10</sup> atoma/om<sup>2</sup> のGr、約 118×15<sup>20</sup> atoma/cm<sup>2</sup> のGa、約 110×16<sup>20</sup> atoma/cm<sup>2</sup> のFeお よび約21×10<sup>20</sup> atoma/cm<sup>2</sup> のMiにより表面が行発 されたシリコンウェハを、第2次に示する極流移

特角平3-208900 (6)

項に投資して独物した結果を同談に示す。 沈浄 快のシリコンウェハは実施例(1) と同様に水洗乾燥し、金属茶均築物質の分析、整粒子再染物質の群定 およびピット状欠略の製造を行った。その結果を発き表に示す。

本発明の請求項(2)の実施例である本発明例 (2)および請求項(3)の実施例である本発明例 (3)は、何れも金属系汚染物質および散粒子汚験 物質が扱めて複談され、かつピット求欠陥もな

比較例のNe.8は形化水素および過酸化水素が少ないため、また比較例のNo.9は悪化水素が少ないためCr. Ca. Feの残存量が多い。比較例のNo.15 は酸化剤の至が少ないためCr. Ca. Feの残容量が多い。また、比較例のNo.16、No.17、No.16 のように弗化水業や過酸化水素の量が多すぎると、ピット次欠陥が現れたり数粒子汚染物質が増加したりする。

# 1 #

	•	•				•	97 I	24	٠. ٠	•		~·	
×o	пиоз.	BF	第三 成 分	<b>技 炒</b> 吟 甜	8 8		後の妄 !#!* eti			茂净安	271	教验子	医分
L	(\$)	(\$)	(85 <sub>4</sub> F)	(#)	(0)	€r	Ca	Fe	Жi	の安面	状次路	79 St.	
91		9.05	# L	300	25	81	2.8	23	KD	х	<b>本</b> し	0	比较份
02	0.10	0.10	セ・レ	300	25	2.4	20	15	15D	<b>A</b>	# L	0	比較例
.93	9.50	5.80	本 し	398.	25	KD	HĐ	Cm.	<b>¥8</b>	0	<b>₽</b> し	•	太克明例1
54	9.80	19-6	なし	360	25	ND.	. ND	<b>X9</b>	NB.	0	<b>☆</b> レ	0	本是明例1
95	0.50	20.3	* L	998	25	80	MD .	115	-NS	0	# L	٥	水是明何1
. 68	8.50	30.0	# L.	300	25	· 100	100	NB,	XD	0	20 13	×	比較別
07	0.58	5.00	0.12	200	25	19	MB .	NĐ.	<b>70</b>		なし	0	本免历的1
	0.50	5.60	# L	390	. 40	EK	#8 ·	10	100	0	# L	.0	木克明例 1
0.9	.0.50	5.00	# L	380	- 60	XD	XD	ND.	NB.	0	± L.	<b>Q</b> .	木角明例 1
10	0.50	6.00	* 1	300	<b>8</b> 0	MD	NO	<b>PD</b>	MO	0	# L	•	未交明例1
11	.15.0	8.10	なし	390	25	DΙΚ	, ND	W8	NO	0	2 L	O.	本免明例1
12	15.1	0.16°	0.15	300	25 ·	<b>68</b>	m)	¥8	и	0	# L	0	水兒男(1)
18	15.0	20.0	# i	300	25	64	ЖĐ	. AD	- AD		なし	0	本発明例1
14	15.0	30.0	4: L	100	25	MB	MB	· 10	<b>96</b>	· <b>O</b> .	8 9	×	比較例
15	25.0	0.05	æ L	200	25	ND	1.8	3,3	60	/ X	# L	0	比较例
16	25.0	0.10	# L	200	25	MD	NĐ	MD	MB	0	2 1	. •	木発男例 1
17	25.0	5-60	* L	300	25	, #D	DB .	120	ND	0	# L	· o	水瓷明例 1
18	25.0	10.0	. a L	799	25	İND	עא	ND	, ND	0	# L	0	本発明例1
19	30.0	5.60	# L	300	25 .	88	NO.	NB.	מו.	0	<b>&amp;</b> 9	0	比较夠
20	38.0	20.0	まし	380	25	119	#9	₽Đ	<b>840</b>	Ö	4 4	Ò	比較夠
21	スダイト	エッチだ	i	309	70	, ND .	2.8	24	316	×	# L	0	夜東例
-22	アンモニ	7 過微化	水黄花	. 860	88	2.7	2.4	77	MD	×	z L	0	<b>英未知</b>
28.	<b>运会通</b>	化水雷油	: .	600	80	HD .	m.	15	NO	×	# L	0	使来的
لــــا	<u> </u>	<u> </u>					1		L			`	

#### 持期平3-208900 (6)

数 2 身

80	195	B <sub>2</sub> O <sub>2</sub>	住化性ガス の組成 (1)	帝三成分	及 持 間 (sec)	报業		· 法净收收函数金属 (×18 <sup>14</sup> etosa/cm²)			-	7 F	菜粒子	区分
	(2)		(3)			(,0)	Ст	Fe	- 31	Q <sub>k</sub>	<b>状欠胎</b>		汚染	. <u></u> .
6,	6.85	1.00	zι.	*L	800	25	. AD	·ND	ND.	KD	4	し	0	水苑明例(2)
92	8.51	0.18	æL	αL	808	25	RD	ND	ND	. No	4	L	0	本務男併(2)
63	0.19	2.01	a L	al	600	25	. MD	, IID	MD.	) KD	4	Ŀ		太亮男狗(2)
	4.50	0.12	<b>\$</b> L	なし	690	25	ND	GK	<b>W</b> 3	3KD	#	L.	0	本竞明殊(2)
<b>45</b>	1.05	9.11	. <b>⊉</b> į.	<b>なし</b> .	360	- 25	ND.	βN	#8	100	#	Ł	0	<b>本発明例(2)</b> .
0.	1.00	1.07	- au	MB.F 0.102	240	25	RB	MĐ.	MD	MD	•	L	٥	本発明例(2)
07	6.93	5.00	AL.	なし .	120	25	ЖÐ	MĐ	ЖO	ND.	#	L	0	本免明例(2)
98	6.63	8.04	#L	なし・	688	25	\$.2	6.8	)XO	5.3	#	Ł	0	比較例
99	0.01	1.00	なし	a L	600	25	13.2	29.4	MD	12.4	22	L	0	比较例
10	9.16	0.29	ØL.	まし	800	49	340	ЖD	) COX	110	*	ı	. 0	水処明例(2)
11	D. 65	東 レ	pars 02	αL	608	25	M	ŊB.	ŒN	MĐ	~	L	o ·	木亮明併(3)
12.	9.15	æ l	80202-2024r	al	800	25	100	NB	·NO	100	=	L	0	太克男伪(3)
23	7.03	a L	2630, -801N <sub>2</sub>	NEAF 0.19%	380	28	蜒	WD	MB	MD.	な	L	0	太岛羽份(3)
16	0.02	æ . ₺	2010 O2	<b>₽</b> L	380	. 25	5.6	45.8	₩B	7.9	本	L	0	比較例
15	0.15	0.01	æι	#L	609	25	8.8	12.4	MD	8.4	<b>Æ</b> .	L	٥	比較例
!8	11.0	7.05	· #L	άl	600	25	199	110	MS	ЖĎ	4	L	×	比較例
17	5.25	10.2	æL ⋅	æL	609	. 25	WĐ	■	#9	MD .	. <b>3</b> 5	ñ	0	比较例
19	11.2	まし	pare O2.	. al	693	. 52	MĐ	<b>88</b>	19	H9	*	43	х	比較例
19	1.00	4 L	2023,0-00237	#L	· B08-	38	MD	жĐ	#0	<b>100</b>	*	し	0	太是明确(2)

## 発明の対策

本発明法によりシリコンウェハを洗浄すると、 全属系汚染物質および教技子汚染物質がともに あて低減された高高体度のシリコンウェハが得ら れ、商化請居技器欠陥の発生やライフタイムの係 下といったシリコンウェハの品質係下が回避され るとともに、ICや LSIなどの高級積化したデバイ スに使用した場合の電気物養劣化のおそれも回避 される。

代理人升理士 井 上 雅 生

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(54) Name of Invention:

Cleaning Method for Silicon Wafer

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# **Specifications**

Name of Invention

Cleaning Method for Silicon Wafer

- Claims 2.
- A method for cleaning a silicon wafer is characterized by a cleaning liquid comprised of an aqueous solution that contains 0.1 - 20 wt% hydrogen fluoride during the silicon wafer cleaning process, along with 0.5
- 25 wt% nitric acid that is used as an oxidizing agent.

- (2) A method for cleaning a silicon wafer is further characterized by a cleaning liquid comprised of an aqueous solution that contains 0.05 10 wt% hydrogen fluoride during the silicon wafer cleaning process, along with 0.05 10 wt% hydrogen peroxide that is used as an oxidizing agent.
- (3) A method for cleaning a silicon wafer is further characterized by a cleaning liquid comprised of an aqueous solution that contains 0.05 10 wt% hydrogen fluoride during the silicon wafer cleaning process, along with oxidizing gas bubbles that are mixed into the solution to be used as an oxidizing agent.

## 3. Detailed Description of the Invention

## **Industrial Field of Application**

This invention pertains to a cleaning method designed to provide a high level of cleanliness along the surface of a silicon wafer.

#### **Prior Art**

In recent years, the high level of integration within devices has brought a strong demand for an improved level of cleanliness along the surface of the silicon wafers that are used as substrates for these devices.

When minute contaminants (also referred to as particles) exist along the surface of a silicon wafer, such as silicon particles, dust, etc., this can result in disconnections and shorts along the wires within a device, and in cases where metallic contaminants exist such as transition metals, other problems can arise such as the occurrence of defects along the oxidation inductive lamination layer, as well as a drop in the lifetime of the device. For this reason, when a cleaning process is conducted for the purpose of removing these contaminants, it is also necessary to prevent contamination during the cleaning process.

Recently, the following methods have been used for cleaning silicon wafers: (1) a method in which cleaning is conducted using a diluted hydrogen fluoride solution, (2) a method in which cleaning is conducted using a mixed solution of either hydrochloric acid or sulfuric acid and hydrogen peroxide, and (3) a method in which cleaning is conducted using a mixed solution of ammonia and hydrogen peroxide. The cleaning liquid used in each of these cleaning methods contains water and a highly pure form of chemicals designed to maximize the reduction of minute particle contaminants and transition metal contaminants.

Among the previous methods noted above, method (1) is capable of dissolving a natural oxide film with a normal thickness of 10Å on a silicon wafer surface, and while this method is highly effective at removing metallic contaminants within the oxide film, it still presents some difficulty when it comes to reducing the level of minute particle contaminants.

Method (2) is able to use a high level of dissolution capability with respect to the metallic contaminants contained within the sulfuric acid, but it is incapable of dissolving an oxide film. For this reason, it is highly effective when it comes to removing metallic contaminants located on top of an oxide film, but it has very little effect when it comes to removing metallic contaminants that are located within an oxide film or along the interface between an oxide film and silicon.

Since method (3) works to dissolve the silicon itself, it is highly effective at removing metallic contaminants located on top of the silicon layer. However, due to the fact that the oxide film that is generated within the basic cleaning solution can easily become embedded with the metallic contaminants, etc., that exist within the cleaning solution, there is a high possibility that the silicon wafer will become contaminated once again. However, due to the fact that this method is highly effective at removing minute particles, it is widely used among wafer manufacturers and device manufacturers.

In addition, as a method for resolving the problems experienced with the prior methods noted above, the so-called Slight Etch method was introduced in which a silicon wafer is cleaned by being dipped into a mixed solution of 60 wt% nitric acid and a maximum of 0.1 wt% hydrogen fluoride. (Ritsuo Takizawa, et al., "Extended Abstracts of Solid State Devices and Materials, 1988, P. 475)

However, highly pure nitric acid, which is referred to as semiconductor grade nitric acid, still contains ppb-order or sub-ppb-order metallic contaminants such as AI, Ca, Cu, Fe, K, Na, Zn, etc. Accordingly, there is a high concentration of metallic contaminants within cleaning solutions that contain a high concentration of nitric acid, such as 60 wt%. Furthermore, when a cleaning tank made of quartz glass is used, the metallic impurities within the quartz glass become eluted into the solution, causing the concentration to gradually increase.

Also, with the high oxidation strength of highly concentrated nitric acid, an oxide film forms on the surface of silicon wafers, and the metallic contaminants within the cleaning solution can easily become

embedded within this oxide film. Therefore, even when the Slight Etch method is applied, there is a limit to the level of high purification that takes place with regard to the silicon wafers.

Problem to Be Solved by the Invention

A method for evaluating the purity of silicon wafer surfaces is one in which the lifetime (hereinafter referred to as the recombination lifetime) is investigated using the microwave reflection method. Using this method, the inventors have evaluated the purity of silicon wafers that were cleaned according to each type of method available. The results showed that in cases where Fe is included in the cleaning solution during cleaning operations in which a mixed solution of ammonia and hydrogen peroxide is used, contamination occurs along the silicon wafer surface at a level of approximately 8 x 10<sup>11</sup> atoms/cm<sup>2</sup> even when the Fe amount is very low at 0.5 ppb. It is further understood that this causes a drop in the recombination lifetime. (Otsuka, et al., The 34<sup>th</sup> Semiconductor and Integrated Circuit Technology Symposium, Preliminary Findings, 1988, P. 37)

The objectives of this invention are as follows: to significantly reduce the level of minute particle contaminants as well as metallic contaminants such as Fe when cleaning silicon wafers; to eliminate quality problems such as the occurrence of defects along the oxidation inductive lamination layer, as well as drops in lifetime; and to obtain a highly pure silicon wafer that will prevent degradation of electrical properties when used in devices.

An outline of this invention follows.

- (1) A method for cleaning a silicon wafer is characterized by a cleaning liquid comprised of an aqueous solution that contains 0.1 20 wt% hydrogen fluoride during the silicon wafer cleaning process, along with 0.5 25 wt% nitric acid that is used as an oxidizing agent.
- (2) A method for cleaning a silicon wafer is further characterized by a cleaning liquid comprised of an aqueous solution that contains 0.05 10 wt% hydrogen fluoride during the silicon wafer cleaning process, along with 0.05 10 wt% hydrogen peroxide that is used as an oxidizing agent.
- (3) A method for cleaning a silicon wafer is further characterized by a cleaning liquid comprised of an aqueous solution that contains 0.05 10 wt% hydrogen fluoride during the silicon wafer cleaning process, along with oxidizing gas bubbles that are mixed into the solution to be used as an oxidizing agent.

This invention is designed to minimize the amount of additives for the purpose of significantly reducing the level of impurities in a cleaning solution when a cleaning operation is conducted for silicon wafers. In addition, a cleaning solution with a superior level of cleaning capability is used. Specifically, this invention calls for an oxidizing agent to be added to a highly acidic aqueous solution containing a minimal amount of fluorine ions. Furthermore, as the oxide film along the silicon wafer surface is dissolved, an etching capability is provided for the silicon, making it possible to effectively remove metallic contaminants such as Fe, etc. Claim (1) notes that a minimal amount of nitric acid is used as an oxidizing agent, whereas Claim (2) notes that a minimal amount of hydrogen peroxide is used, and Claim (3) notes that an oxidizing gas is used.

According to this invention, the respective concentrations of hydrogen fluoride, nitric acid, and hydrogen peroxide within the cleaning solution are given in weight percentages of HF, HNO<sub>3</sub>, and H<sub>2</sub>O<sub>2</sub>. In Claim (3), it is possible to use an oxidizing gas that contains oxygen as well as nitrous oxide (dinitrogen monoxide). Furthermore, an ultrapure form of water is used as a solvent.

In Claim (1), given less than 0.1 wt% of hydrogen fluoride and less than 0.5 wt% of nitric acid, the removal effect with regard to the metallic contaminants is insufficient. If the hydrogen fluoride concentration is increased to exceed 20 wt%, a trend is recognized in which the amount of minute particle contaminants increases along the surface of the silicon wafers. Furthermore, if the nitric acid concentration is increased to exceed 25 wt%, there is an excessive amount of etching along the silicon surface, resulting in a defective wafer surface with a cloudy appearance. Thus, if the maximum concentration of hydrogen fluoride is set to 20 wt% and the maximum concentration of nitric acid is set to 25 wt%, there is no substantial problem with regard to the concentration of impurities that become intermixed from the chemicals.

Therefore, the concentration of hydrogen fluoride has been set to a range of 0.1 - 20 wt%, and that of nitric acid has been set to a range of 0.5 - 25 wt%. Note that if the cleaning solution temperature is allowed to increase beyond the required level, this will cause the hydrogen fluoride as well as the water and nitric acid to escape in the form of steam and may result in a cleaning solution that falls outside the scope prescribed by the invention. Furthermore, increasing the temperature requires more time, which could result in a significant loss of productivity. Therefore, the preferred maximum temperature is  $80^{\circ}$ C.

In Claim (2), given less than 0.05 wt% of hydrogen fluoride and less than 0.05 wt% of hydrogen peroxide, the removal effect with regard to the metallic contaminants is insufficient. If the hydrogen fluoride concentration is increased to exceed 10 wt%, a trend is recognized in which the amount of minute particle contaminants increases along the surface of the silicon wafers. Furthermore, if the hydrogen peroxide concentration is increased to exceed 10 wt%, there is an excessive amount of etching along the silicon surface, resulting in a defective wafer surface with a cloudy appearance. Thus, if the maximum concentration of hydrogen fluoride is set to 10 wt% and the maximum concentration of hydrogen peroxide is set to 10 wt%, there is no substantial problem with regard to the concentration of impurities that become intermixed from the chemicals.

Therefore, the concentration of hydrogen fluoride has been set to a range of 0.05 – 10 wt%, and that of hydrogen peroxide has been set to a range of 0.05 – 10 wt%. Note that if the cleaning solution temperature is allowed to increase beyond 80°C, this will cause uneven cleaning such that pits may form on the silicon wafer surface after the heat treatment is conducted. Therefore, the preferred maximum temperature is 80°C.

In Claim (3), given less than 0.05 wt% of hydrogen fluoride and no intermixing of oxidizing gas bubbles, the removal effect with regard to the metallic contaminants is insufficient. If the hydrogen fluoride concentration is increased to exceed 10 wt%, the amount of minute particle contaminants increases along the surface of the silicon wafers, and at the same time, the etching amount becomes excessive, resulting in a defective wafer surface. Thus, if the maximum concentration of hydrogen fluoride is set to 10 wt%, there is no substantial problem with regard to the concentration of impurities that become intermixed from the chemicals. Furthermore, since a highly pure form of an oxidizing gas can be relatively easily obtained which has a very low concentration of impurities, this poses no problem.

Therefore, the concentration of hydrogen fluoride has been set to a range of 0.05 – 10 wt%, and oxidizing gas bubbles are intermixed to be used as an oxidizing agent. Note that if the cleaning solution temperature is allowed to increase beyond 80°C, this will cause uneven cleaning such that pits may form on the silicon wafer surface after the heat treatment is conducted. Therefore, the preferred maximum temperature is 80°C.

In order to intermix the oxidizing gas bubbles within the cleaning solution, it is possible to use a means that is already well-known, such as inserting a gas introduction tube into the cleaning tank or installing gas jets along the bottom of the cleaning tank such that the gas is allowed to bubble into the tank.

Based on this invention, there is an electrochemical coupling between the anodic dissolution reaction of the silicon that occurs between the silicon and fluorine ions, and the cathodic reaction that is caused by the oxidizing agent, resulting in a movement of the corrosion potential to the anode side. This makes it easy to remove the metallic contaminants from the silicon wafer surface.

Passive membranes comprised of silicon oxides are either chemically or electrochemically dissolved within the highly acidic aqueous solution containing fluorine ions that fall within the scope of the method discussed in this invention. Due to the fact that this will cause stripping of the silicon wafer surface, it is necessary to add a certain amount of oxidizing agent, and when the corrosion potential moves to the anode side, the metal contaminants are easily removed from the wafer surface.

Note that according to the method described in this invention, substances other than those noted above as components of the cleaning solution may also be added without causing a loss of cleaning capability. Examples include salt types such as ammonium fluoride, etc.

In addition, according to the method of this invention, it is also acceptable to use prior well-known forms of cleaning methods in conjunction with this method. As an example, for greater effect, cleaning can be conducted using a mixed solution of ammonia and hydrogen peroxide, followed by another cleaning in which a diluted fluorine aqueous solution is used, after which cleaning is finally conducted using the method of this invention.

## **Embodiments**

## <1> Embodiment for Claim 1

The surfaces of silicon wafers are contaminated with the following: approx. 270 x 10<sup>10</sup> atoms/cm<sup>2</sup> of Cr, approx. 240 x 10<sup>10</sup> atoms/cm<sup>2</sup> of Cu, approx. 2230 x 10<sup>10</sup> atoms/cm<sup>2</sup> of Fe, and approx. 313 x 10<sup>10</sup> atoms/cm<sup>2</sup> of Ni. These wafers are then dipped into the various cleaning solutions listed in Table 1, which provides the results for each cleaning. Immediately after cleaning, the silicon wafers are cleaned twice for at least five minutes each under ultrapure running water, after which they are spun dry and an analysis is conducted to determine the level of metallic contamination on the surface.

During the analysis, chemical etching using a concentrated fluorine and nitric acid solution is applied to dissolve a 1  $\mu$ m surface layer, after which the metallic element concentration within this solution is measured using a frameless atomic absorption photometry analysis method. Note that ND indicates a level that falls below the lower limit for analytical determination. Also note that Cr is less than 0.1 x  $10^{10}$  atoms/cm<sup>2</sup>, Cu and Fe are less than  $0.2 \times 10^{10}$  atoms/cm<sup>2</sup>, and Ni is less than  $2.0 \times 10^{10}$  atoms/cm<sup>2</sup>.

The minute particles on the wafer surface are measured using a wafer surface particulate measuring device, and those wafers showing 10 particulates per wafer or less are indicated with an O, whereas those showing more than 10 particulates per wafer are indicated with an X.

In addition, a visual judgment is made as to whether the wafer surfaces after cleaning are hydrophobic or hydrophilic. Those that are hydrophobic are indicated with an O, those that are slightly hydrophobic are marked with a  $\Delta$ , and those that are hydrophilic are marked with an X. A hydrophobic surface indicates that a silicon oxide, namely and oxide layer, does not exist on the silicon wafer surface.

An optical microscope is then used in order to observe whether or not there are any pitting defects along the wafer surface, and the findings are included in the table. The absence of pits indicates that the etching amount is appropriate, such that the wafer has an extremely smooth mirror surface.

In Table 1, Comparison Examples 1 and 15 show that the residual amounts of Fe and Cu are particularly high due to the low levels of hydrogen fluoride during cleaning. In the same fashion, Comparison Examples 6 and 14 show a high occurrence of pitting as well as residual minute particle contamination due to the fact that the hydrogen fluoride levels are too high. Pitting defects also occur in the cases of Comparison Examples 19 and 20 due to the fact that the nitric oxide levels are too high.

Prior Art Example No. 21 in which the Slight Etch cleaning method is applied uses an aqueous solution that has 60 wt% of HNO3 and 0.1 wt% of HF, but the removal effect is low with regard to Fe. Prior Art Example No. 22 in which the Ammonia Hydrogen Peroxide cleaning method is applied uses an aqueous solution that has 4.1 wt% of NH<sub>3</sub> and 4.4 wt% of H<sub>2</sub>O<sub>2</sub>, and among the various cleaning methods, this one has the lowest removal effect with regard to metallic contaminants; especially in the case of Fe. Prior Art Example No. 23 in which the Chlorine Hydrogen Peroxide cleaning method is applied uses an aqueous solution that has 5.1 wt% of HCl and 4.4 wt% of H<sub>2</sub>O<sub>2</sub>, and although this method is currently the most widely used due to its metallic contaminant removal effect, it still has a low removal effect with regard to Fe when compared to the examples given for this invention.

Example (1) of this invention shows a significant reduction in both minute particle contaminants as well as metallic contaminants, with no evidence of pitting defects on the surface after cleaning. Furthermore, the

surface is shown to be hydrophobic after cleaning, with no existence of an oxide film. This means that the type of recontamination that occurs when cleaning is performed in such a way that an oxide film is formed during cleaning and metallic contaminants within the cleaning solution are allowed to become embedded within the oxide film has not occurred in the case of Example 1 of this invention.

## Embodiments for Claims 2 and 3

The surfaces of silicon wafers are contaminated with the following: approx. 18 x 10<sup>10</sup> atoms/cm<sup>2</sup> of Cr, approx. 110 x 10<sup>10</sup> atoms/cm<sup>2</sup> of Cu, approx. 110 x 10<sup>10</sup> atoms/cm<sup>2</sup> of Fe, and approx. 21 x 10<sup>10</sup> atoms/cm<sup>2</sup> of Ni. These wafers are then dipped into the various cleaning solutions listed in Table 2, which provides the results for each cleaning. The cleaned wafers then undergo the same procedures as noted in Embodiment <1> with regard to water rinsing and drying, followed by an analysis of the metallic contaminants, measurements regarding minute particle contaminants, and observations of pitting defects. The results are shown in Table 2.

Examples (2) and (3) of this invention, which are the respective embodiments of Claims (2) and (3) of this invention, show that the levels of metallic contaminants and minute particle contaminants are drastically reduced, with no evidence of pitting defects.

Due to the low levels of hydrogen fluoride and hydrogen peroxide used during cleaning in the case of Comparison Example No. 8, as well as the low level of hydrogen fluoride used during cleaning in the case of Comparison Example No. 9, both of these examples show high residual amounts of Cr, Cu, and Fe. In the case of Comparison Example No. 15, the low level of oxidizing agent used during cleaning results in high residual amounts of Cr, Cu, and Fe. Also, as shown in Comparison Examples No. 16, No. 17, and No. 18, excessive amounts of hydrogen fluoride and hydrogen peroxide result in the appearance of pitting defects as well as an increase in the level of minute particle contaminants.

Table 1

			•	·		1 at	ie i						
			Third	Clean-			y metal co						
•	HNO <sub>3</sub>	HF	Com-	ing	Sol.		urface aft			Surface		Min.	
No.			po-	Time	Temp.		(x 10 <sup>10</sup> at	oms/cm <sup>2</sup> )	)	After	Pitting	Part.	Class.
•	(%)	(%)	nent	(sec.)	(°C)	ŀ				Cleaning	Defects	Cont.	
			(NH₄F)	·		Cr	Cu	Fe	Ni				
01	0.50	0.05	None	300	25	61	2.3	23	ND	X	None	0	CE
02	0.10	0.10	None	300	25	2.4	20	· 15 ·	ND	Δ	None	0	CE
03	0.50	5.00	None	300	25	ND	ND	ND	ND	0	None	0	PE1
04	0.50	10.0	None	300	25	ND	ND	ND	ND	0	None	0	PE1
. 05	0.50	20.0	None	300	25	ND	ND	ND	ND	O.	None	. <b>O</b>	PE1
06	0.50	30.0	None	300	25	ND	ND	ND	ND.	0	Yes	X	CE _
07.	0.50	5.00	0.1%	300	25	ND .	ND	ND	ND	O-	None	. 0	PE1
08	0.50	5.00	None	300	40	ND	ND	ND ·	ND	. O	None	0	PE1
.09	0.50	5.00	None	300	60	. ND	ND	ND.	ND	0.	None	0	PE1 ·
10	0.50	5.00	None	300	80	ND ·	ND	ND.	ND	0	None	O	PE1
1.1	15.0	0.10	None	300	25	ND	ND	· ND	ND	.0	None	Ο ·	PE1
12	15.0	0.10	0.1%	300	25	ND	ND	ND	ND	0	None	. 0	PE1

13	15.0	20.0	None	300	· 25	ND	ND	ND	ND	Ο.	None	0	PE1
14	15.0	30.0	None	300	25	ND	ND	ND	ND	0	Yes	Χ.	CE
15	25.0	0.05	None	300	25	ND	1.8	. 3.3	ND	X	None	0	CE
16	25.0	0.10	None	300	25 ,	. ND	ND	ND	ND	0	None ·	0	PE1
· 17	25.0	· 5.00	None	300	25	ND-	ND	ND.	ND ·	0	None	0	PE1
18	25.0	10.0	None	300	25	ND	ND	ND	ND	0	None	0	PEI
19	30.0	5.00	None	300	· 25	ND	ND	ND ·	ND	0	Yes	0	CE ·
20	30.0	20.0	None	300	25	ND	ND	· ND	ND .	0	Yes	0	CE
21	Sligh	nt Etch M	ethod	300	.70	ND	2.8	34	ND	X	None	0	PAE
22	Amn	onia Hyd	rogen	600	80	2.7.	2.4	77	ND	X	None	0	PAE
•	Per	oxide Me	thod .	•			<u> </u>			-			
23	Chlo	rine Hyd	rogen	600	· 80	ND	ND	15	ND ·	X	None	0	PAE
·		oxide Me			·	<u> </u>			<u> </u>		<u> </u>	<u> </u>	

[Translator's Note: In the Classification (Class.) column above, CE = Comparison Example; PE1 = Patent Example (1); PAE = Prior Art Example]

Table 2

		<del></del>	<del>` </del>	i		r	77						1
			Oxidiz	774	Class				ontaminat er cleanii				1 .
				Third	Clean-						1		1
·			ing	Com-	ing	Sol.		(x 10° at	oms/cm <sup>2</sup> )	)	D	Min.	
No.	HF	H <sub>2</sub> O <sub>2</sub> ∶	Gas	po-	Time	Temp.	.•		•		Pitting	Part.	Class.
			Com-	·				<del>,</del>	,				1
	(%)	(%)	posi-	nent	(sec.)	(°C)	_	_	·	_	Defects	Cont.	
			tion				Cr	Fe	Ni.	Cu			ļ ''
	·		(%)	·									
01	0.05	1.00	None	None	600	25	ND	ND	· ND	ND	None	0	PE2
02	0.51	0.10	None	None	600	25	ND	ND	ND	ND	None	0	PE2
03	0.10	2.01	None	None	600	25	ND:	ND	ND	ND	None	.0	PE2
04	0.50	0.12	None	None	600	25	ND	ND	ND	ND	None	0	PE2
05	1.05	0.11	None	None	360	25	ND	ND	ND	. ND	None	0	PE2
06	1.00	1.07	None	NH₄F	240	25	ND	ND	ND	ND	None	О	PE2
		ŀ		0.10%									
07	0.99	5.00	None	None	120	25	ND	ND	ND	. ND	None	0	PE2
08	0.03	0.04	None	None	600	25	8.2	6.8	ND	5.3	None	. 0	CE
09	0.01	1.00	None	None	600	25	ND	.23.4	ND	12.4	None	0	CE .
10.	0.10	0.20	None	None	600	40	ND	ND ·	ND	ND	None	0	PE2
11	0.05	None	Pure O <sub>2</sub>	None	600	25	ND	ND	ND	ND ·	None	Ο,	PE3
12	0.15	None	80%O <sub>2</sub> + 20%Ar	None	600	25	ND	ND	ND	ND	None	0	PE3
13 -	1.01	None	20%O <sub>2</sub> +80%N <sub>2</sub>	NH <sub>4</sub> F	360	. 30	ND	ND	ND	, ND	None	0	PE3
	0.00	<del></del>		0.10%		. 05	MD	45.0	NTO	7.9	None		CE
14	0.02	None	Pure O <sub>2</sub>	None	360	25	ND	45.8	ND		None	.0	<del></del>
15	0.15	0.01	None	None	600	25	ND	12.4	ND	8.4	None	0	CE
. 16	11.0	2.05	None	None	600	25	ND .	ND	ND	ND	None	X	CE
17	5.95	10.2	None	. None	600	25	ND	ND	ND	ND	Yes	0	CE
18	11.2	None	Pure O <sub>2</sub>	None	600	25	ND	ND	ND	ND	Yes	X.	CE
19	1.00	None	20%N <sub>2</sub> O + 80%N <sub>2</sub>	None	600	30	ND	ND	ND	ND	None	.0	PE3

[Translator's Note: In the Classification (Class.) column above, CE = Comparison Example; PE2 = Patent Example (2); PE3 = Patent Example (3)]

#### Effect of the Invention

When a silicon wafer is cleaned using the method described in this invention, a highly pure silicon wafer can be obtained in which the levels of metallic contaminants and minute particle contaminants are significantly reduced. Furthermore, not only does this invention make it possible to avoid a drop in quality among silicon wafers, such as the occurrence of defects along the oxidation inductive lamination layer as well as a drop in lifetime, when these wafers are used in highly integrated devices such as IC, LSI, etc., it is also possible to prevent degradation of electrical properties in these devices.

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